] î0 5r • KAWASAKI STEEL GIHO Vol. 22(1990) No.3

Ü ½ " Ô î ± • î#Ý Ü "; © Ù å É Þ î ° F A Ü A"I f ¹5ð G b6ä\$Î

Development of Grooved Flat- Bar Steels for the Reaction Plates of Linear Motor Cars Ø ù (Hiroyuki Hayashi)

0[":

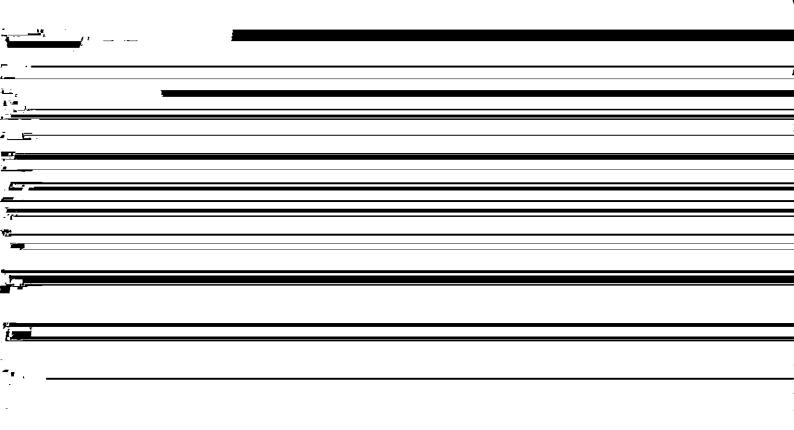
ܽ"Ôî#ÝÜ"; ©ÙåÉÞî°†04 M•Su_>*"ÝÑȆ5ðÈ_KœM•Sub"å•îÎå»2†]î5 d 4' &k\¹ [6ä\$ÎKS 5ðÈb/²8 _ AÏb‰ @È8"ÜA†!Õ6ë} [BgM•G\cT7´\l€Z8S@>*ÉÛ«³©åÔ¹Ý\!Õ6ë5ðÔ¹Ýb%Ê'2?}"ÜAgB@•+ [6•G\†0b KS G€† μ _4:#ÝK2.0mm èVbœîÂîÁå¢5†wM•¹5ð@"}€S rS)œŠb9×8Ü";©Ùå ÉÞî°†04 M•Sub"ÜA•8'\"ÝÑÈ':²4Š•8'†4:G(V_'ö#.K>*"ÜAÆ_'M_"Ýц~6IO•04•/;†&'gKS

Synopsis:

A method that permits jointing of aluminum plates and steel plates as key material for the manufacture of reacti on plates for linear motor cars has been developed by Kawasaki Steel jointly with Kawasaki Heavy Industries, Ltd. Hot forming of overhang grooves, with their opening narrower than their beds, on the steel plate surface was virtually impossible. But a study using Plasticine models and hot -rolled steel models paved the way for this new method called the anchor -bonding. By applying it to commercial -scale mills, flat bars having an overhang beyond 2.0 mm have been successfully obtained. With a technology also e stablished to control cross- sectional areas of both overhang groove and aluminum projection within proper range, the resultant uniform filling of aluminum within the overhang grooves assures the manufacture of reaction plates of yet higher bonding.

(c)JFE Steel Corporation, 2003

•ec blîa?} 70t[ArM



Development of Grooved Flat-Bar Steels for the Reaction Plates of Linear Motor Cars







要旨

リニアモータカー用リアクションプレートを製造するために、アルミ板を網板に終合するためのファルードンとはないできません。

Ē

突条部を充塡し、機械的に結合させるもので、この結合力がリアク Soft material Hard material ¥ さらにリアクションプ<u>レートには</u>気健に F X 温度亦ル L ※ 資産

海にトスジュニル発動も呼い。 マット4C2 MM4

•		
ž:•		· · · · · · · · · · · · · · · · · · ·
	3.1 最適突起形状	幅も大きくすると,溝底の部分でオーバーラップを生じている
		(No. 4 および No. 5)。これらの結果から, 圧下前の突起の幅寸法を
· /-	<u>港</u> 両側の空記は次丁程のロールドトス甲下で港の内面側に <u>郊</u> 形十	以展り 45mm 45mm 45mm 15mm 15mm 15mm 15mm 15mm
3,		
.1		
•		
-		
,		
·		
-		
	る。このときの圧下は突起部のみであることから、断面全体の長手	また突起部分は平ロールで圧下されるときに溝の内外面に変形が
Y_1	古典の恋歌はいまりはたり 内担はこの様士内、ただがいエン・・	of the contract to the second contract of the second contract of the contract
	, <u> </u>	
		
, —		
•		
<u>-</u>	\ <u>1</u>	
<u> </u>		
n		
ئــــه		
- <u>1</u>		
* ±		
·		
- <u>-</u> -		
<u>í. </u>		
-		

Į,

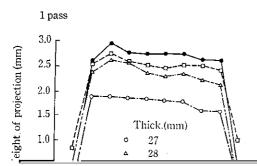


Table 2 Experimental conditions of hot rolling

Rolling mill	2 Hi rolling mill			
Roll dimensions	290 ¢mm dia., 300 mm length			
Material*1				
Standard	SS 41			
Dimension (mm)	$34 t \times 100 W \times 250 L \times 10 H$ of projection			
	$34 t \times 100 W \times 250 L \times 10 H$ of projection $38 t \times 100 W \times 250 L \times 6 H$ of projection			
Method of forming	① One pass of flat roll			
	② Two pass of flat roll			

_	nnn	α = 56.3°	Na 1 ralihna	ある。 そのため実機での生産に際しては下記の点を考慮する必要があっ
- - -				•
<u>,</u>				
;				
i k		_		
1.				
<u> </u>				
	A			
•				
ni		1.		
· -	777777	$\alpha = 35.8$ °	No.2 caliber	- (2) 幅方向端部の突起は幅方向のメタルフローを考慮し、幅方向中央部の突起以上の高さが得られること。 (3) カリバーへの誘導がよいこと。
'	1 //~	, , , , , , , , , , , , , , , , , , , 		And A submitting to a submitted to contract the submitted to the submitted tof the submitted to the submitted to the submitted to the submitte
<u> </u>				
. ል: ታ 				
# # # # # # # # # # # # # # # # # # #				
- 				
		<u></u>	-	
		— → F.		
<u> </u>				
 1	<u> </u>			1
_ _	-			

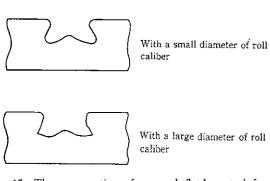
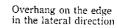
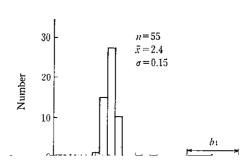
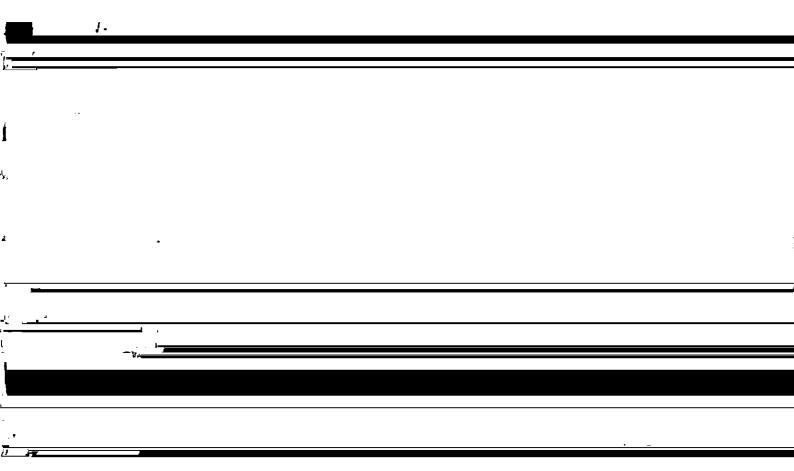


Fig. 15 The cross-section of grooved flat-bar steel formed







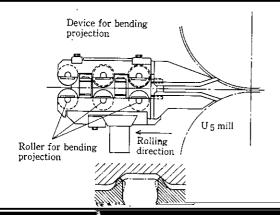


Fig. 17 Example of the quantity of overhang (b_1-b_2) of commercially produced steel flat-bars

Table 4 Rolling reduction mill load and plate thickness during the rolling for bonding extruded aluminum shape to grooved flat-bar steel

Aluminium Total Rolling Draft